



The issue of dissertation and its current state

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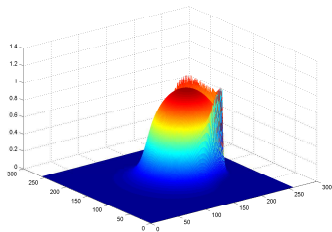
Czech Republic



Institute of Machine
and Industrial Design

Outline

- ▶ Introduction
- ▶ Mathematical model
- ▶ Numerical algorithm
- ▶ Results
- ▶ Conclusion and future work



Title:

Advanced Solver of Elasto-hydrodynamic Problems

Supervisor:

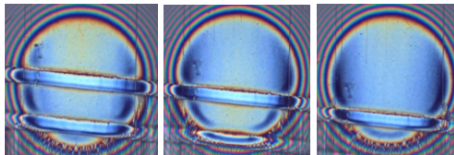
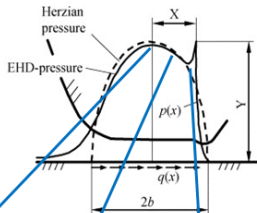
prof. Ing. Martin Hartl, Ph.D.

Aim of dissertation

- ▶ Stable and fast numerical solver for elasto-hydrodynamic (EHL) problems (steady state and transient solution)
- ▶ Incorporate to the solver artificial roughness and non-Newtonian model of the lubricant
- ▶ Comparison with experiments

Deformation of roughness in rolling/sliding EHL contact

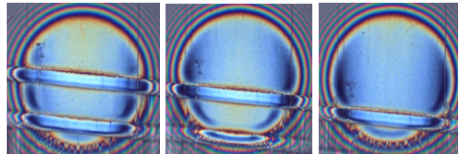
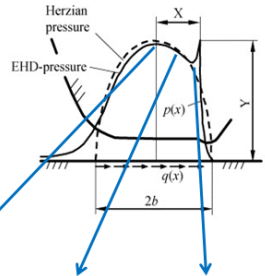
- ▶ study of surface roughness
 - experimental (Kaneta, 1992; Wedeven et al., 1978)
 - numerical (Lee, 1990; Chang 1991)
- ▶ effect of operating conditions on the roughness (Venner et al., 1995)
- ▶ amplitude reduction model (Hooke, 2005; Lubrecht et al., 1999) - introducing a single parameter
- ▶ Non-Newtonian lubricant response (Felix-Quinonez, 2004)



Deformation of roughness in rolling/sliding EHL contact

- ▶ Lubricant non-newtonian response
- ▶ Low sliding conditions: appropriate lubricant rheology model?
- ▶ High sliding conditions: limiting shear stress

$$\tau_L = \Lambda p$$



Reynolds equation

$$\frac{\partial}{\partial x} \left(\frac{\rho h^3 \eta_x}{12\eta} \frac{\partial p}{\partial x} \right) + \frac{\partial}{\partial y} \left(\frac{\rho h^3 \eta_y}{12\eta} \frac{\partial p}{\partial y} \right) - u_m \frac{\partial(\rho h)}{\partial x} - \frac{\partial(\rho h)}{\partial t} = 0$$

Film thickness equation

$$h(x, y, t) = h_0(t) + \frac{x^2}{2R_x} + \frac{y^2}{2R_y} - R(x, y, t) + \frac{2}{\pi E_r} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{p(x', y') dx' dy'}{\sqrt{(x-x')^2 + (y-y')^2}}$$

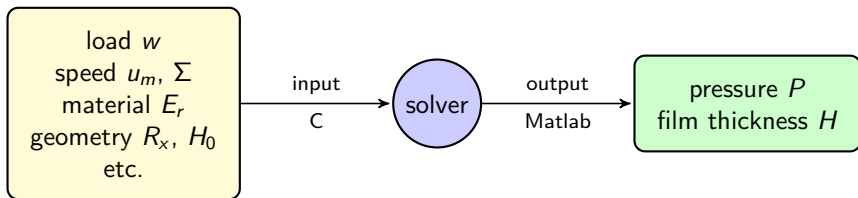
- ▶ force balance equation
- ▶ pressure-viscosity relation
- ▶ pressure-density relation

- ▶ **1. EHL smooth contact + Newtonian fluid model**
- ▶ **2. EHL non-smooth contact (dent, ridge, ...) + Newtonian fluid model**
- ▶ **3. EHL smooth contact + Non-Newtonian (Eyring) model**
- ▶ **4. EHL non-smooth contact under Non-Newtonian conditions**
- ▶ **5. Non-Newtonian models: limiting shear stress, ...**

Algorithm

The model is solved in programming language C, and visualization of the solution is provided in Matlab.

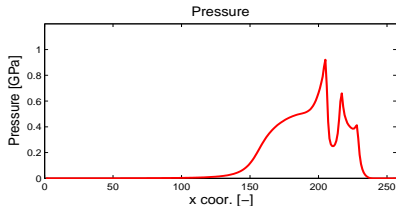
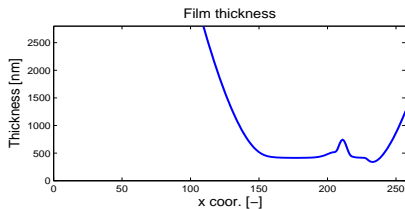
- ▶ domain up to 1025×1025 discrete points
- ▶ residuals up to $\mathcal{O}(10^{-9})$



Surface feature type - Dent

$$R(x, y, t) = \begin{cases} \frac{h_{dent}}{2} (1 + \cos(\pi r)) & \text{if } r \leq 1 \\ 0 & \text{else} \end{cases}$$

$$r = \sqrt{\left(\frac{x-x_0 - \frac{u_1}{u_m} t}{l_x}\right)^2 + \left(\frac{y}{l_y}\right)^2}$$



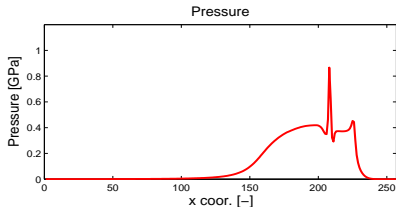
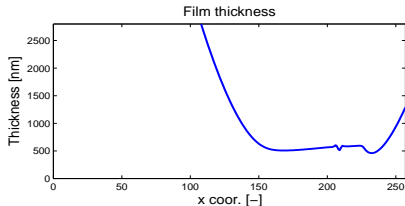
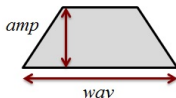
Dent

$w = 27N$, $u_m = 0.15m/s$, $\Sigma = 0$, $\alpha = 22GPa^{-1}$, $\eta_0 = 0.421Pas$,
 $E_r = 123.8GPa$, etc.

Surface feature - transverse ridge

$$R(x, y, t) = amp \left(10 \frac{-10r^2}{wav^2} \right) \cos \left(\frac{2\pi r}{wav} \right) - 0.4amp \left(10 \frac{-10r^2}{0.25wav^2} \right) \cos \left(\frac{2\pi r}{0.5wav} \right)$$

$$r = x - x_0 - \frac{u_1}{u_m} t$$



Transverse ridge

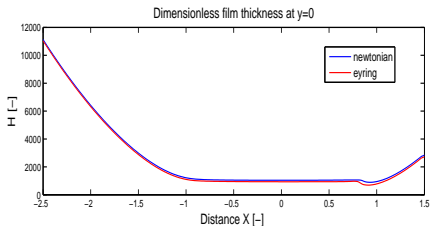
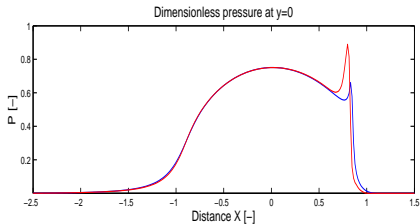
$w = 49.9N$, $u_m = 0.2m/s$, $\Sigma = 1$, $\alpha = 23.6GPa^{-1}$, $\eta_0 = 0.2016Pas$,
 $E_r = 123.8GPa$, etc.

Newtonian vs. Eyring fluid model

- ▶ incorporating variables η_x and η_y into Reynolds equation

- ▶ rheological function

$$f\left(\frac{\tau}{\tau_0}\right) = \frac{\tau_0}{\tau} \sinh\left(\frac{\tau}{\tau_0}\right)$$



Conclusion and future work

- ▶ work continues on developing the numerical solver:
 - Eyring model
 - rheology models: limiting shear stress, Rabinowitsch model (Chapkov, 2006)
- ▶ time steps - 2nd order discretization scheme
- ▶ join roughness solver with non-newtonian model



Thank for your attention.